Real-Time Sensor-Based Feedback Control for Obstacle Avoidance in Unknown Environments

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Introduction

Global approaches

- Navigation functions (Koditschek et al., 1990).
- Navigation transform (Loizou, 2017).
- Hybrid feedback (Sanfelice et al., 2006; Berkane et al., 2019; Casau et al., 2019; Berkane et al., 2021).

Local approaches

- Artificial potential fields (Khatib, 1986; Koditschek et al., 1990).
- Extended navigation functions (Lionis et al., 2007; Filippidis et al., 2011).
- Separating hyperplanes (Arslan et al., 2019).
- Navigation through safety velocity cones (Berkane, 2021).



- Navigate unknown environments filled with obstacle.
- Objective: design a sensor-based feedback control to ensure safe navigation.

Notations and Definitions

Reach of sets

The skeleton $\mathbf{Sk}(\mathcal{A})$:

 $\mathbf{Sk}(\mathcal{A}) := \{ x \in \mathbb{R}^n : \mathbf{card}(\mathbf{P}_{\overline{\mathcal{A}}}(x)) > 1 \}.$

The reach of \mathcal{A} at $x \in \overline{\mathcal{A}}$ is defined as

$$\begin{split} \mathbf{reach}(\mathcal{A}, x) &:= \\ \left\{ \begin{array}{ll} 0, & x \in \partial \overline{\mathcal{A}} \cap \overline{\mathbf{Sk}(\mathcal{A})}, \\ \sup\{r > 0: \mathbf{Sk}(\mathcal{A}) \cap \mathcal{B}(x, r) = \emptyset\}, \\ & \text{otherwise.} \end{array} \right. \end{split}$$

The reach of the set \mathcal{A} is given by

$$\operatorname{reach}(\mathcal{A}) := \inf_{x \in \mathcal{A}} \{\operatorname{reach}(\mathcal{A}, x)\}.$$

The set \mathcal{A} has **positive reach** if $\mathbf{reach}(\mathcal{A}) > 0$.



Sets of class $\mathcal{C}^{k,l}$

- $k \in \mathbb{N}$: the differentiability order.
- $l \in [0,1]$: is the Hölder continuity.
- If l = 0: the kth derivative is bounded.
- If l = 1: the kth derivative is Lipschitz continuous.

Notations and Definitions

Tangent cone

We denote by $\mathbf{T}_{\mathcal{A}}(x)$ the **tangent cone** to \mathcal{A} at a point $x \in \mathbb{R}^n$, and is given by

$$\mathbf{T}_{\mathcal{A}}(x) = \left\{ z \in \mathbb{R}^{n} : \\ \lim_{\tau \to 0^{+}} \frac{\mathbf{d}_{\mathcal{A}}(x + \tau z)}{\tau} = 0 \right\}.$$

Nagumo's theorem

Consider the system $\dot{x} = f(x)$. For each initial condition $x(0) \in \mathcal{X}$, where \mathcal{X} is a closed set, we assume that the system admits a unique solution. Then the set \mathcal{X} is forward invariant if and only if

$f(x) \in \mathbf{T}_{\mathcal{X}}(x), \forall x \in \mathcal{X}.$



Figure: Tangent cones and Nagumo's Theorem Application.

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Workspace - Free Space



- Workspace \mathcal{W} : closed subset of the Euclidean space \mathbb{R}^n .
- Obstacles \mathcal{O}_i , i = 1, ..., M: open subsets in \mathbb{R}^n strictly contained in \mathcal{W} .
- Free space \mathcal{X} : a subset in \mathbb{R}^n ,

$$\mathcal{X} := \mathcal{W} \setminus \bigcup_{i=1}^{M} \mathcal{O}_i.$$
 (1)

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Workspace - Free Space

Assumption 1

The set \mathcal{X} has a **positive reach**, *i.e.*,

$$\operatorname{reach}(\mathcal{X}) > 0.$$
 (2)

In other words, there exists a positive real h > 0 such that any point $x \in \mathcal{X}$, with $\mathbf{d}_{\mathbf{C}\mathcal{X}}(x) < h$, has a unique projection $\mathbf{P}_{\partial\mathcal{X}}(x)$.



If Assumption 1 holds, then

$$\mathbf{d}_{\mathcal{O}_i,\mathcal{O}_j} > 2h, \quad \forall i,j \in \mathbb{M} \text{ with } i \neq j,$$
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Workspace - Practical Free Space

- Consider a ball-shaped robot with a radius R and centred at $x \in \mathbb{R}^n$.
- Let
 e be a positive real and satisfies the following inequality:

$$0 < R < \epsilon < h. \tag{4}$$

• We define the **practical free space** as follows:

$$\mathcal{X}_{\epsilon} := \{ x \in \mathbb{R}^n : \mathbf{b}_{\mathcal{C}\mathcal{X}}(x) \ge \epsilon \} \subset \mathcal{X}.$$
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Dynamical System

We consider the first-order robot dynamics

$$\dot{x} = u, \qquad u \in \mathbb{R}^n.$$
 (6)

- The robot is operating in the free space X and restricted to stay in the **practical free space** X_€.
- Let x_d be the **goal** position.

Objectives

finding $u = \kappa(x, x_d, \mathcal{X}_{\epsilon})$, such that:

- κ is locally Lipschitz continuous.
- κ is sensor-based.
- safety is guaranteed, *i.e.*, x must stay in \mathcal{X}_{ϵ} .
- the robot's position is asymptotically stabilized at x_d.

For the sake of simplicity, $\kappa(x, x_d, \mathcal{X}_{\epsilon})$ will be written as $\kappa(x)$.

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Feedback Control Design

To ensure safety, we apply Nagumo's theorem, *i.e.*, we need

$$u \in \mathbf{T}_{\mathcal{X}_{\epsilon}}(x), \quad \forall x \in \mathcal{X}_{\epsilon}.$$
 (7)

- To guarantee **convergence**, one must keep u as close as possible to the **nominal controller** κ_0 .
- This consists of solving the nearest point problem formulated as follows

 $\min_{u} ||u - \kappa_0(x)||^2 \text{ subject to } u \in \mathsf{T}_{\mathcal{X}_{\epsilon}}(x), \forall x \in \mathcal{X}_{\epsilon}, \qquad (8)$

The solution for u to this optimization problem is equivalent to finding the projection of the nominal control $\kappa_0(x)$ onto the tangent cone $\mathbf{T}_{\mathcal{X}_{\epsilon}}(x)$.

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- To guarantee convergence, one must keep u as close as possible to the nominal controller κ₀.
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Feedback Control Design

• When $x \in int(\mathcal{X}_{\epsilon})$:

• The tangent cone $\mathbf{T}_{\mathcal{X}_{\epsilon}}(x) \equiv \mathbb{R}^{n}$.

• When $x \in \partial \mathcal{X}_{\epsilon}$:

- For CX ≠ {Ø}, with a positive reach h, CX_e is a set of class C^{1,1} and the boundary ∂X_e is a C^{1,1}-submanifold of dimension (n − 1).^a
- The tangent cone is given by the half-space

 $\mathbf{T}_{\mathcal{X}_{\epsilon}}(x) = \{ z \in \mathbb{R}^{n} : v(x)^{\top} z \leq 0 \} \\ \forall x \in \partial \mathcal{X}_{\epsilon}, \quad (9)$

v(x): is the outward normal unit vector associated to each $x \in \partial X_{\epsilon}$



Figure: Tangent cone for smooth boundary sets.

⁴Michel C Delfour and J-P Zolésio. Shapes and geometries: metrics, analysis lifferential calculus, and optimization. SIAM, 2011.

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Feedback Control Design

• The projection $\mathbf{P}(\kappa_0(x), \mathbf{T}_{\mathcal{X}_{\epsilon}}(x))$ is unique.

• When $v(x)^{\top} \kappa_0(x) > 0$, the projection reduces to the orthogonal projection onto the hyperplane $v(x)^{\top} z = 0$, which is given by

$$\Pi (v (x)) \kappa_0 (x) := \left(\mathbf{I}_n - v (x) v (x)^\top \right) \kappa_0 (x). \quad (10)$$



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Feedback Control Design

The resulting control law that solves the *nearest point problem* is given by

$$u = \kappa(x) = \begin{cases} \kappa_0(x), & x \in \mathsf{int}(\mathcal{X}_\epsilon) \text{ or } v(x)^\top \kappa_0(x) \le 0, \\ \Pi(x)\kappa_0(0), & x \in \partial \mathcal{X}_\epsilon \text{ and } v(x)^\top \kappa_0(x) \ge 0. \end{cases}$$
(11)



Feedback Control Design

• Knowing that $v(x) = -\nabla \mathbf{b}_{\mathcal{CX}}(x)$, $\forall x \in \partial \mathcal{X}_{\epsilon}$, we can rewrite the controller in terms of the distance function

$$\kappa(x) = \begin{cases} \kappa_0(x), & \mathbf{b}_{\mathsf{C}\mathcal{X}}(x) > \epsilon \text{ or } \kappa_0(x)^\top \nabla \mathbf{b}_{\mathsf{C}\mathcal{X}}(x) \ge 0, \\ \Pi(x) \kappa_0(x), & \mathbf{b}_{\mathsf{C}\mathcal{X}}(x) = \epsilon \text{ and } \kappa_0(x)^\top \nabla \mathbf{b}_{\mathsf{C}\mathcal{X}}(x) \le 0, \end{cases}$$
(12)

■ This controller is a piecewise continuous vector field with a discontinuity at the boundary ∂X_e of the practical free space.



Figure: Resulting trajectory under the piecewise continuous controller.

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■ This controller is a piecewise continuous vector field with a discontinuity at the boundary ∂X_ϵ of the practical free space.



Figure: Resulting trajectory under the piecewise continuous controller.

Feedback Control Design

The smoothed version of the controller is given by

$$\kappa(x) = \begin{cases} \kappa_{0}(x), & \mathbf{b}_{\mathbf{C}\mathcal{X}}(x) > \epsilon' \text{ or } \kappa_{0}(x)^{\top} \nabla \mathbf{b}_{\mathbf{C}\mathcal{X}}(x) \ge 0, \\ \hat{\Pi}(x) \kappa_{0}(x), & \mathbf{b}_{\mathbf{C}\mathcal{X}}(x) \le \epsilon' \text{ and } \kappa_{0}(x)^{\top} \nabla \mathbf{b}_{\mathbf{C}\mathcal{X}}(x) \le 0, \end{cases}$$
(13)

where $0 < R < \epsilon < \epsilon' \leq h$ and

$$\widehat{\Pi}(x) := \mathbf{I}_n - \phi(x) \nabla \mathbf{b}_{\mathbf{C}\mathcal{X}}(x) \nabla \mathbf{b}_{\mathbf{C}\mathcal{X}}(x)^{\top},$$
(14)

$$\phi(x) := \min\left(1, \frac{\epsilon' - \mathbf{b}_{\mathcal{C}\mathcal{X}}(x)}{\epsilon' - \epsilon}\right).$$
(15)



Figure: Resulting trajectory under the smooth controller.

Safety Analysis

Lemma 1

We assume the free space \mathcal{X} is a set of class $\mathcal{C}^{2,l}$, where $0 \leq l \leq 1$. Consider the practical free space set \mathcal{X}_{ϵ} . Then, the smoothed control $\kappa(x)$ is **locally Lipschitz-continuous**.

Theorem 2 (Safety)

Consider the set $\mathcal{X} \subset \mathbb{R}^n$ that describes the free space. Consider the set $\mathcal{X}_{\epsilon} \in \mathbb{R}^n$ that describes the practical free space. Consider the closed-loop system under the locally Lipschitz-continuous control law $\kappa(\cdot)$. Then,

- the closed-loop system admits a unique solution and,
- the set \mathcal{X}_{ϵ} is **forward invariant**.

The forward invariance of \mathcal{X}_{ϵ} is equivalent to the safety of the robot.

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- the closed-loop system admits a unique solution and,
- the set \mathcal{X}_{ϵ} is forward invariant.
- The forward invariance of \mathcal{X}_{ϵ} is equivalent to the safety of the robot.

Stablity Analysis

We a consider the following nominal controller

$$\kappa_0(x) = -k(x - x_d), \quad k > 0.$$
(16)

Theorem 3 (Stability)

Under the nominal controller $\kappa_0(.)$ given by (16), we have

- the distance $||x x_d||$ is non-increasing,
- the equilibrium point $x = x_d$ is locally exponentially stable, and
- and trajectories converge to the set $\mathcal{E} \cup \{x_d\}$, where

$$\mathcal{E} := \{ x : \mathbf{b}_{\mathcal{C}\mathcal{X}}(x) = \epsilon, (x - x_d) = \lambda \nabla \mathbf{b}_{\mathcal{C}\mathcal{X}}(x), \lambda \in \mathbb{R}_{>0} \}$$
(17)

is a set of measure zero.

■ The nature of the undesired equilibria defined by the set *E* is directly related to the topology of the obstacles.

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Topology Of The Obstacle Set

We suppose all obstacles are convex.



Figure: (Left) shows a non-convex obstacle for which the trajectory of the robot converges to the undesired equilibrium, and (right) shows a convex obstacle for which the trajectory converges to the desired goal x_d .

Topology Of The Obstacle Set - Strong Convexity Condition

Assumption 2 (Strong Convexity)

The Jacobian matrix $\mathbf{J}_{\mathbf{P}_{\partial \mathcal{X}}}(x)$ of the metric projection of any stationary point $x \in \mathcal{E}$ onto the boundary $\partial \mathcal{X}$ of the free-space satisfy

$$\mathbf{J}_{\mathbf{P}_{\partial \mathcal{X}}}\left(x\right) \prec \frac{||x_d - \mathbf{P}_{\partial \mathcal{X}}(x)||}{\epsilon + ||x_d - \mathbf{P}_{\partial \mathcal{X}}(x)||} \mathbf{I}_n, \quad \forall x \in \mathcal{X},$$
(18)



Figure: Visualization of Assumption 3: (left) shows an obstacle that doesn't meet the assumption. (Right) shows an obstacle that satisfies the assumption.

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(18)



Figure: (Left) shows a flat obstacle, as viewed from the position of the vehicle, for which its trajectory converges to the undesired equilibrium.(Right) shows a strongly convex obstacle where the trajectory converges to the desired goal x_d .

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Topology of the Obstacle Set - AGAS

Theorem 3

In addition, if Assumption 3 holds, then

- 1 all the undesired equilibria $\bar{x} \in \mathcal{E}$ are unstable, and
- **2** the desired equilibrium x_d is locally exponentially stable and **almost** globally asymptotically stable.

Numerical Simulation 2D

Numerical Simulation 3D

- Smooth feedback control law that guarantees safe navigation.
- Ensure AGAS under some topological conditions.
- Sensor-based and computationally efficient controller.

Future works:

- Relaxing the strong convexity assumption.
- Extending to higher-order dynamics.

Thank You!