Position, Velocity, Attitude and Gyro-Bias Estimation from IMU and Position Information

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Problem Formulation



 $\dot{p} = v,$ $\dot{v} = g + Ra_B,$ $\dot{R} = R[\omega]_{\times},$



Apparent acceleration a_I = Ra_B is unknown → we need to estimate it as well for use in the attitude observer

Translational Dynamics

Let
$$x := (p, v, a_I) \in \mathbb{R}^9$$
.

$$\dot{x} = Ax + B_1g + B_2\dot{a}_l$$
$$y = C(t)x$$

$$A = \begin{bmatrix} 0 & I & 0 \\ 0 & 0 & I \\ 0 & 0 & 0 \end{bmatrix}, B_1 := \begin{bmatrix} 0 \\ I \\ 0 \end{bmatrix}, B_2 := \begin{bmatrix} 0 \\ 0 \\ I \end{bmatrix}, C(t) = \begin{bmatrix} C_{\rho}(t) \\ 0 \\ 0 \end{bmatrix}^{\top}$$

Linear system with unknown input *a_I*

• We only measure $a_B = R^{\top} a_I$

Translational Motion Observer

Consider the "quasi-linear" observer

$$\begin{cases} \hat{x} = \hat{z} + B_2 \hat{R} a_B \\ \dot{\hat{z}} = A \hat{x} + B_1 g + K(t)(y - C(t) \hat{x}) + \sigma_1(\hat{R}) \end{cases}$$

with $\sigma_1(\hat{R}) \rightarrow 0$ when $\hat{R} \rightarrow R$ (note that $\hat{R}a_B \rightarrow a_I$).

• If $\hat{R} \equiv R$, this is equivalent to the **Luenberger-type observer**

$$\dot{\hat{x}} = A\hat{x} + B_1g + B_2\dot{a}_I + K(t)(y - C(t)\hat{x})$$

►
$$K(t) = \gamma L_{\gamma} P(t) C(t)^{\top} Q(t)$$
, with $\gamma \ge 1$,
 $L_{\gamma} = \text{blockdiag}(I_3, \gamma I_3, \gamma^2 I_3)$ and $P(t)$ is solution of the CRE
 $\frac{1}{\gamma} \dot{P} = AP + PA^{\top} - PC(t)^{\top} Q(t)C(t)P + V(t)$,

Rotational Motion Observer

Consider the "nonlinear complementary filter"-type observer¹

$$\begin{cases} \dot{\hat{R}} &= \hat{R}[\omega^{y} - \hat{b}_{\omega} + k_{1}\sigma_{2}]_{\times} \\ \dot{\hat{b}}_{\omega} &= \mathbf{Proj}(\hat{b}_{\omega}, -k_{2}\sigma_{2}) \end{cases}$$

$$\sigma_2 = \rho_1(m_B \times \hat{R}^\top m_I) + \rho_2(a_B \times \hat{R}^\top \operatorname{sat}(\hat{a}_I))$$

- Proj: is the parameter projection function
- sat: is a saturation function

¹R. Mahony, T. Hamel and J. Pflimlin, "Nonlinear Complementary Filters on the Special Orthogonal Group," in IEEE TAC, 2008. H. F. Grip, T. I. Fossen, T. A. Johansen and A. Saberi, "Attitude Estimation Using Biased Gyro and Vector Measurements With Time-Varying Reference Vectors," in IEEE TAC, 2012.

Main Result

Assumption

- Pair $(A, C(\cdot))$ is uniformly observable
- m_l and $a_l(t)$ are not collinear for all times
- $\omega, b_{\omega}, a_I, \dot{a}_I$ are uniformly bounded

Theorem (Semi-global exponential stability)

For all initial conditions (except attitude errors at 180°), there exist (high) gains such that the estimation error converges exponentially to zero.

Although, sufficiently large gains are needed in the proof, simulation results demonstrate that this is very conservative.

Full position measurement in the inertial frame (e.g., GPS)



 $C_p = I_{3\times 3}$

7/18

Range measurements (e.g., Ultra-wide-Band (UWB))



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At least 4 non-coplanar source points are needed located at p_i .

$$d_i = \|p - p_i\|, \quad i = 1, \cdots, n.$$

Output equaion:

$$y_i := \frac{1}{2} \left(d_i^2 - d_1^2 - \|p_i\|^2 + \|p_1\|^2 \right), \quad i = 2, \cdots, n.$$

$$y = \begin{bmatrix} (\rho_1 - \rho_2)^\top \\ \vdots \\ (\rho_1 - \rho_n)^\top \end{bmatrix} \rho := C_\rho \rho$$
(1)

Bearing measurements in the inertial frame



Bearing measurements in the inertial frame

$$b_i = R_i^{\top} \frac{p - p_i}{\|p - p_i\|}, \quad i = 1, \cdots, n,$$

- ▶ $R_i \in SO(3)$: Orientation of camera *i* w.r.t. the inertial frame.
- *p_i*: Position of camera *i* in the inertial frame.

Note that

an

$$\Pi(b_i)R_i^\top(p-p_i)=0$$

where $\Pi(z) := I - \frac{zz^{\top}}{\|z\|^2}$ is the orthogonal projection. • Therefore,

$$y_i := \Pi(b_i) R_i^\top p_i = \Pi(b_i) R_i^\top p$$

d letting $y = (y_1, \dots, y_n)$ we have
$$y = \begin{bmatrix} \Pi(b_1) R_1^\top \\ \vdots \\ \Pi(b_n) R_n^\top \end{bmatrix} p := C_p(t) p.$$

11/18

Bearing measurements

Lemma (Uniform observability)

(A, C(t)) is uniformly observable if there exist $\delta, \mu > 0$ such that for all $t \ge 0$ one has

$$rac{1}{\delta}\int_t^{t+\delta}\sum_{i=1}^n\Pi(R_ib_i(s))ds\geq \mu I_3.$$

- Single camera: Vehicle is never static nor moving on a straight line passing through the camera.
- **Two cameras:** Vehicle not aligned (indefinitely) with both cameras.
- Three cameras or more: If at least 3 cameras are not aligned, the observability condition is always satisfied.

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Altimeter

• An altimeter is a sensor that measures the altitude

 $y = [0 \ 0 \ 1]p.$

Lemma (Uniform observability: bearings+altimeter) (A, C(t)) is uniformly observable if there exist $\delta, \mu > 0$ such that for all $t \ge 0$ one has

$$rac{1}{\delta}\int_t^{t+\delta}\sum_{i=1}^n\Pi(R_ib_i(s))ds+e_3e_3^ op\geq\mu I_3.$$

- Single camera + altimeter: Vehicle not moving at the same altitude as the camera or, if doing so, not moving on a straight line passing through the camera
- Two cameras + altimeter: Cameras not at the same altitude. If the cameras are at the same altitude, vehicle must not be aligned (indefinitely) with both cameras.

Simulations: true trajectory



Figure 1: True trajectory of the vehicle.

Simulations: single bearing



Figure 2: Observability holds but slow convergence.

Simulations: single bearing + altimeter



Figure 3: Stronger observability.

Conclusion

- A generic navigation observer with semi-global exponential stability
- Position information (full, bearings, range) in the inertial frame
- Future work using information in the body-frame (e.g., on-board cameras)

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Thank you

Questions?

18/18